

MATLAB-Based Predictive Computational Models for Turbine Blade Failure Analysis and Mechanical Behaviour in High-Performance Engines

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ABSTRACT

High-performance gas turbines are central to aerospace and power generation industries, necessitating advanced designs to withstand extreme thermal and mechanical stresses. This study develops a comprehensive computational framework using MATLAB to simulate turbine blade behaviour and predict failure modes under high-pressure gas turbine engine (HPGTE) conditions. The methodology incorporates modular simulation of individual engine components including compressor, combustor, turbine, and exhaust stages within a MATLAB-based GUI. Key parameters such as pressure ratios, temperature variations, and mass flow are modelled, with validation performed through comparison with industry benchmarks. Additionally, the framework employs parametric studies and random test condition generation to analyse the influence of blade count, rotor and hub radii, air density, design velocity, and tip-speed ratio on power output and structural integrity. Results highlight that optimized turbine designs with lower blade counts, larger rotor radii, high design velocities, and minimized hub radii closely approach the theoretical Betz limit for power capture, while also ensuring enhanced durability against mechanical and thermal stresses. The study underscores the significance of predictive computational models in proactive maintenance and design refinement, paving the way for further research in dynamic loading simulations, advanced fatigue modelling, and real-time performance monitoring.

Keywords: *High-Pressure Gas Turbine Engine (HPGTE), Optimized Turbine Designs, MATLAB.*

1. INTRODUCTION

The demand for high-performance gas turbines has escalated in recent decades, driven by advancements in aerospace and power generation technologies [1]. These engines must operate efficiently at higher temperatures and speeds while maintaining reliability and longevity, making turbine blades subjected to extreme thermal and mechanical conditions pivotal to overall performance [2]. Predicting blade failure is crucial for safety and cost-effectiveness [3], motivating the development of predictive computational models aimed at mitigating the risks associated with premature failure [4]. In gas turbines, blades experience complex mechanical stresses centrifugal forces from high rotation, aerodynamic forces from hot gas flow, and thermal stresses due to rapid temperature fluctuations [5]. Understanding these stress interactions is vital for designing durable components [6]. Traditional testing methods, while informative, can be expensive, time-consuming, and carry safety concerns [7]. Through contrast, predictive modelling offers a virtual testbed to simulate real-world conditions and evaluate performance without extensive physical prototyping [8]. Techniques such as Finite Element Analysis (FEA) have thus become integral in assessing blade integrity under various stresses.

Developing predictive models for turbine blade failure requires integrating material properties, mechanical loads, and environmental factors [9]. High-performance blades, often fashioned from nickel-based superalloys, are remarkably strong at elevated temperatures yet still prone to fatigue, creep, and thermal fatigue [10]. Accounting for each failure mechanism demands a unified approach that combines classical analytical methods with advanced computational techniques. MATLAB's specialized toolboxes and robust numerical solvers facilitate this integration, enabling detailed simulations of turbine blade behaviour under operational extremes. Through MATLAB-based FEA, fatigue analyses, and optimization algorithms, engineers can accurately predict blade responses, identify probable failure points, and propose design or material modifications. Additionally, machine learning models such as neural networks can be trained on simulation data to produce probabilistic failure estimates, supporting proactive maintenance and repair strategies. The result is a more thorough and cost-effective approach to turbine blade design. Predictive computational models also allow engineers to explore a wide range of design scenarios, material choices, and operating conditions before finalizing a solution. Such flexibility leads to improved optimization for specific applications, enhancing blade durability and efficiency [11]. Moreover, the ability to forecast failures before they occur supports proactive maintenance, reducing overall lifecycle costs and increasing operational safety. Through embedding these models into the design, testing, and maintenance processes, the aerospace and power generation industries can drive continuous innovation in turbine technology while minimizing risks tied to blade failure.

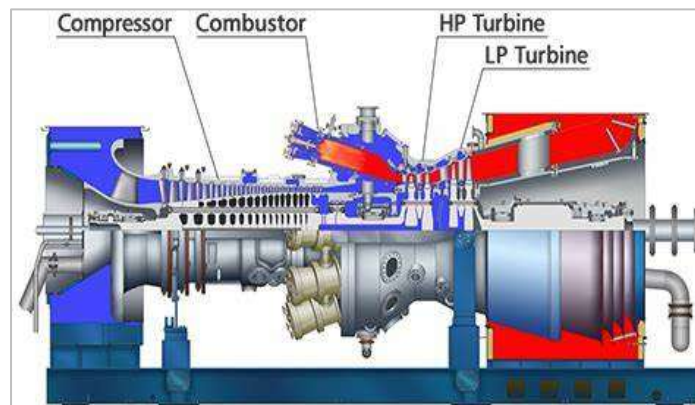


Figure 1

Source: <https://power.mhi.com/products/gasturbines/lineup/h100/>

The gas turbine operates through four main stages: intake, compression, combustion, and exhaust. Air enters through the intake and is compressed to high pressure in the compressor. This compressed air is mixed with fuel and ignited in the combustor, generating high-temperature, high-pressure gases. These gases expand through the high-pressure (HP) and low-pressure (LP) turbines, producing rotational energy that drives the compressor and an external load, such as a generator or propulsion system. The remaining energy is expelled through the exhaust, creating thrust or additional power. This efficient energy conversion process is widely used in aerospace and power generation applications.

1.1 High-Performance Gas Turbines: The Engine of Modern Industry

1.1.1 The Growing Demand for High-Performance Gas Turbines

The global demand for high-performance gas turbines has surged due to several factors, including rapid advancements in aerospace, energy production, and military technologies. Gas turbines, which are the heart of many modern propulsion and power systems, need to operate efficiently under extreme conditions. High temperatures, high rotational speeds, and high mechanical loads are standard challenges that these turbines face in their operational environments. In industries such as aerospace and power generation, the ability to achieve higher efficiency and reliability while withstanding these challenging operational environments is becoming increasingly important [12, 13].

In aerospace applications, for instance, the demand for more fuel-efficient engines drives the need for turbines capable of enduring high temperatures and delivering maximum power with minimum weight. The aviation industry, particularly, relies on gas turbines to deliver thrust at the lowest possible weight while optimizing fuel efficiency. Similarly, in the power generation sector, gas turbines are often used in combined-cycle power plants, where their efficiency can determine the economic feasibility of electricity generation, especially with rising global demand for sustainable energy.

1.1.2 The Role of Gas Turbines in Aerospace and Power Generation

Gas turbines are widely used in aerospace propulsion systems, such as jet engines, and power generation systems, including electricity-producing plants. In aerospace, turbine engines like turbojets, turbofans, and turboprops provide thrust for aircraft propulsion. The technological advancements in material science and computational engineering have allowed turbines to achieve significant performance gains, but these systems are often operating at the edge of their mechanical limits due to the demanding operational conditions they face.

In power generation, gas turbines play a critical role in both standalone plants and combined-cycle systems. Combined-cycle plants use the exhaust heat from the gas turbines to produce steam, which powers a steam turbine, further increasing efficiency. These turbines are required to operate reliably over long periods, making reliability and longevity critical for economic feasibility in power production [14].

1.1.3 Advances in Cooling Technology for Turbine Blades

One of the key tests in high-performance gas turbine operation is managing the heat generated within the engine. Cooling systems are essential for preventing the turbine blades and other components from reaching temperatures that could lead to material degradation or failure [15-18]. Several advanced cooling technologies have been developed to address this issue, including internal cooling channels, thermal barrier coatings, and film cooling. Internal cooling channels allow coolant to circulate within the blades, absorbing heat and carrying it away from critical areas. Thermal barrier coatings, often made from ceramics, provide a layer of insulation between the hot gases and the turbine blade surface, reducing the amount of heat transferred to the material [19-21]. These cooling technologies have significantly improved the performance and lifespan of gas turbines, allowing them to operate at higher temperatures without sacrificing reliability.

1.1.4 Turbine Blade Design Optimization

The optimization of turbine blade design is another critical area for enhancing the performance of high-performance gas turbines. The shape and aerodynamics of the turbine blades must be carefully engineered to maximize efficiency while minimizing operational stresses [22]. CFD simulations are commonly used to model airflow over turbine blades and refine their geometry for optimal performance. Through adjusting the geometry and material properties based on simulation data, engineers can significantly improve turbine efficiency and extend the operational lifespan of the engine [23].

1.1.5 The Role of Maintenance and Monitoring in Ensuring Reliability

Maintenance and monitoring are essential for ensuring the continued performance and reliability of high-performance gas turbines. Given the extreme conditions under which these turbines operate, regular maintenance is necessary to prevent unexpected failures and ensure that the turbine continues to function efficiently [24]. Turbine blade inspection is a critical component of this process, as blades are subject to wear, cracking, and other forms of damage over time.

Advances in monitoring technologies, such as vibration sensors and temperature monitoring systems, enable real-time detection of potential issues. These systems provide early warnings of impending failures, allowing maintenance teams to address problems before they escalate into catastrophic breakdowns. Additionally, predictive maintenance models built on historical data and real-time monitoring inputs can anticipate when turbine blades require repair or replacement, thereby minimizing downtime and maximizing overall efficiency [25].

1.1.6 Environmental Considerations and Sustainability

As the demand for energy continues to rise, the environmental impact of gas turbines has become an increasingly significant consideration. Efforts to improve turbine efficiency have direct environmental benefits by reducing fuel consumption and lowering emissions [26]. However, the development of high-performance gas turbines must also address the broader sustainability challenges associated with their use. These efforts include the development of turbines that can operate on cleaner fuels, such as natural gas and hydrogen, as well as the integration of carbon capture technologies into power generation systems. By improving the environmental performance of gas turbines, the aerospace and energy sectors can play a pivotal role in mitigating the effects of climate change and reducing their overall carbon footprint.

1.1.7 The Future of High-Performance Gas Turbines

The future of high-performance gas turbines is poised to be shaped by continued advancements in materials science, cooling technologies, and computational modelling. The ongoing push for greater efficiency and reduced environmental impact will drive innovation in turbine design and operation [27]. As computational tools—such as finite element analysis (FEA) and computational fluid dynamics (CFD)—continue to evolve, engineers will be able to design even more efficient and reliable turbines that can operate under even more extreme conditions.

In addition to technological progress, the integration of machine learning and artificial intelligence will further enhance the ability to predict and optimize turbine performance. Predictive maintenance models, leveraging large datasets and real-time monitoring, will help extend the lifespan of gas turbines and reduce downtime [28]. These developments ensure that high-performance gas turbines remain well-positioned to meet the growing demands of the aerospace, power generation, and military sectors in the years ahead.

1.2 Introduction to Turbine Blade Mechanics

Gas turbines are crucial components in modern aerospace and power generation industries. They must be capable of withstanding high temperatures, mechanical stresses, and extreme environmental conditions. Due to the intense operating environment, turbine blades are subjected to a variety of complex mechanical stresses, including centrifugal forces, aerodynamic forces, and thermal stresses [29]. Understanding the mechanical behaviour of turbine blades is crucial to ensuring the engine operates efficiently and reliably over its lifespan. This requires in-depth knowledge of how the materials and geometry of turbine blades respond to these stresses [30]. In this section, we will

explore the key mechanical stresses acting on turbine blades, their effects on turbine performance, and the mechanisms that allow turbine blades to survive in such extreme conditions.

1.2.1 The Function of Turbine Blades in a Gas Turbine Engine

Turbine blades serve as the interface between the hot gases generated by the combustion process and the mechanical systems that convert this thermal energy into rotational energy. In a gas turbine engine, hot combustion gases flow over the turbine blades, causing them to spin and drive the compressor and other engine components. These blades must withstand exceptionally high temperatures often exceeding 1,500°C in modern engines and immense centrifugal forces due to high rotational speeds. Additionally, aerodynamic forces from the gas flow contribute significantly to the overall stress profile on each blade. Consequently, turbine blades are manufactured from specialized high-performance materials that can endure such extreme conditions without experiencing fatigue, creep, or failure.

1.2.2 Key Mechanical Stresses Acting on Turbine Blades

Turbine blades experience three main types of mechanical stresses:

Centrifugal Forces: The turbine blades experience centrifugal forces due to their rapid rotational motion. At high speeds, these forces become substantial and can lead to deformation, fatigue, and failure of the blades if not properly accounted for in the design.

Aerodynamic Forces: As the hot gases pass over the blades, they exert aerodynamic forces on the blades, including lift, drag, and pressure distribution. These forces are influenced by the design and geometry of the blades, the angle of attack, and the flow characteristics of the gases. Aerodynamic forces can cause bending, torsion, and vibration in the blades.

Thermal Stresses: Thermal stresses arise from the temperature gradients across the turbine blade, particularly when the blade is exposed to high-temperature combustion gases. The variation in temperature from the leading edge to the trailing edge of the blade induces thermal expansion, creating internal stresses that can lead to deformation, cracking, and eventually failure.

1.3 Centrifugal Forces and Their Impact on Turbine Blade Mechanics

1.3.1 The Nature of Centrifugal Forces

Centrifugal forces are generated due to the rotational motion of the turbine blades. As the turbine spins at high rotational speeds, the blades are subject to a centrifugal force that acts outward from the centre of rotation. The magnitude of this force increases with the speed of rotation and the mass of the blades. In high-performance gas turbines, blades can reach rotational speeds of up to 15,000 revolutions per minute (RPM), making centrifugal forces a significant factor in turbine blade mechanics.

The centrifugal force F_c on a turbine blade equals its mass m multiplied by the square of the angular velocity ω^2 and by the distance from the centre of rotation r . In other words:

Centrifugal Force = Mass \times (Angular Velocity)² \times Radius

$$F_c = m \cdot \omega^2 \cdot r$$

This force acts to pull the turbine blades outward, creating tensile stresses along the length of the blade. As a result, the blade material is subjected to stretching, and the centrifugal force can cause permanent deformation if the blade is not properly designed [31].

2. RESEARCH METHODOLOGY

2.1 Objective and Hypothesis of Study

Objectives

- 1) To study various design for High-Pressure Gas Turbine Engine (HPGTE) in present research.
- 2) To establish various parameters for model that unifies thermodynamic and structural analyses to assess turbine blade performance under extreme conditions.
- 3) To develop a modular computational framework for simulating High-Pressure Gas Turbine Engine (HPGTE) components in MATLAB.
- 4) To perform various real time and Compare simulation results with industry benchmarks to refine blade geometry, tip-speed ratios, and other critical factors for maximum efficiency and durability.

Hypothesis

- 1) A MATLAB-based thermodynamic–structural model for HPGTE accurately predicts blade performance under extreme conditions and aligns with industry benchmarks.
- 2) Parametric optimization of blade geometry and operating parameters significantly boosts engine efficiency and durability beyond conventional methods.

2.2 Research Methodology

The research methodology for developing and analysing a high-pressure gas turbine engine (HPGTE) simulation focuses on a computational and experimental approach. This involves creating mathematical models, developing code to simulate thermodynamic processes, and analysing outputs for validation and improvement. The methodology is divided into phases, including problem definition, modelling, computational implementation, validation, and performance analysis. Each phase incorporates principles of thermodynamics, numerical modelling, and control systems to ensure accuracy and reliability in the results. Tools like MATLAB and GUIDE (Graphical User Interface Development Environment) provide the foundation for both simulation and user interaction with the model [125].

Problem Definition: The first phase of the methodology involves identifying the scope of the HPGTE system. The research seeks to simulate the thermodynamic processes of various components, including the inlet, compressor, combustor, turbine, and exhaust. Key challenges include accurate modelling of pressure, temperature, and mass flow variations. Additionally, real-world inefficiencies, such as mechanical losses and non-ideal pressure ratios, must be incorporated. The objectives are to calculate outlet conditions for each stage, determine work and efficiency, and analyse trends under varying input parameters, such as mass flow rate, efficiency, and pressure ratios. This phase defines clear research questions and objectives.

Modelling Thermodynamic Processes: A robust mathematical model is central to this research. The turbine, compressor, combustor, and exhaust systems are modelled using thermodynamic equations. For instance, the compressor process uses the isentropic efficiency formula to calculate temperature and pressure changes. The combustor's model incorporates heat addition and pressure losses, while the turbine process accounts for work extraction and mechanical efficiency. Conservation of mass and energy principles guide the calculations, ensuring that mass flow and energy remain balanced. These equations are implemented for each stage, enabling comprehensive simulations of the HPGTE system. The models incorporate both ideal and non-ideal conditions [126].

Developing the Computational Framework: The simulation is implemented in MATLAB due to its powerful mathematical and graphical capabilities. The project uses MATLAB's GUIDE to develop a user-friendly interface. Functions such as Compressor Function, Combustor Function, Turbine Function, and Exhaust Function define the behaviour of individual components. The user interface allows users to input parameters like pressure ratios, efficiencies, and mass flow rates, which feed into the mathematical models. The code includes validation steps, such as input error checks and warnings for non-physical results. Outputs include temperature, pressure, and mass flow variations, as well as graphical visualizations for easy interpretation.

Validation of Models: Parameters such as temperature and pressure ratios at each stage are cross-referenced with industry-standard values. Discrepancies are analysed, and models are refined to improve accuracy. For example, isentropic efficiency assumptions are adjusted based on the validation data. Additionally, boundary conditions are tested to ensure the simulation produces realistic results under extreme operating conditions. Sensitivity analysis is also conducted to identify parameters that significantly affect outputs.

Sensitivity Analysis: Parameters such as pressure ratio, isentropic efficiency, and fuel heating value are varied within realistic ranges. The resulting changes in temperature, pressure, and work output are analysed. This process identifies which parameters have the greatest influence on engine performance, providing insights into design optimizations. For instance, increasing the compressor's pressure ratio improves overall efficiency but may result in higher turbine inlet temperatures. Sensitivity analysis ensures the model's robustness and provides valuable data for future design improvements.

Graphical Analysis and Visualization: Graphical analysis is used to visualize the performance trends of the HPGTE system. MATLAB plots illustrate variations in pressure, temperature, and mass flow across engine stages. For example, pressure and temperature rise in the compressor and combustor and drop in the turbine and exhaust are shown graphically. The GUI integrates toggle switches to enable or disable specific graphs, such as pressure vs. stage or temperature vs. stage. These visualizations help users intuitively understand the simulation results and identify any anomalies in the output. Effective graphical representation is critical for analysing complex systems like HPGTE [127].

Input Parameter Validation: The methodology incorporates robust input validation to ensure meaningful and realistic simulation results. Constraints on user inputs, such as ensuring efficiency values are between 0 and 1 and pressure ratios are positive, prevent computational errors and non-physical outputs. Additionally, the system warns users if unrealistic parameters, such as negative work output or temperatures, are detected. This validation step ensures the integrity of the simulation and enhances the user experience. For example, fuel heating value checks ensure accurate combustion calculations, while specific heat capacity validations prevent errors in energy calculations.

Pressure and Temperature Analysis: Pressure and temperature variations are critical for analysing engine performance. The methodology computes stage-by-stage variations, starting from the inlet through to the exhaust. For each stage, the simulation calculates outlet pressure and temperature using thermodynamic relationships, accounting for isentropic and mechanical efficiencies. These calculations help determine the overall efficiency of the engine and its ability to perform under varying conditions. For instance, the combustor's pressure loss and heat addition significantly influence turbine inlet conditions. These analyses provide insights into how different components contribute to the general performance of the HPGTE system.

Performance Metrics: The research evaluates several performance metrics, including thermal efficiency, specific fuel consumption, and thrust. Specific fuel ingesting measures the fuel required to generate thrust, providing a benchmark for fuel efficiency. Thrust is calculated by analysing the exhaust stage and the difference in momentum across the system. These metrics help assess the feasibility of the HPGTE design and identify areas for improvement. For example, optimizing the turbine's efficiency reduces specific fuel consumption, thereby improving overall performance [128].

Iterative Model Refinement: The methodology includes iterative refinement of the models based on the simulation results. Discrepancies between predicted and expected results are analysed to identify inaccuracies in the model assumptions or equations. For example, initial simulations might assume ideal gas behaviour, which can be refined to incorporate real gas effects for higher accuracy. Additionally, the refinement process involves incorporating feedback from validation studies and sensitivity analyses. Each iteration improves the model's ability to predict real-world performance, ensuring the simulation is both accurate and reliable for design and analysis purposes.

Experimental Data Integration: Where possible, experimental data from actual gas turbine engines is integrated into the simulation for validation and calibration. Data such as pressure, temperature, and mass flow at key stages are compared with simulation outputs. This integration ensures that the models accurately reflect real-world engine behaviour. Any significant deviations between experimental and simulated results are investigated, and the models are adjusted accordingly. Experimental data also provides benchmarks for evaluating the simulation's accuracy and serves as a basis for further improvements in the modelling approach.

Implementation Challenges: Several challenges are addressed during the implementation phase. For instance, achieving numerical stability in the simulation requires careful handling of edge cases, such as extreme pressure or temperature conditions. Additionally, ensuring the user interface is intuitive and robust involves significant effort in GUI design. Computational efficiency is another challenge, as the simulation must process complex equations while maintaining fast response times. These challenges are mitigated through rigorous testing, code optimization, and user feedback. Overcoming these challenges ensures that the final simulation tool is both reliable and user-friendly [129, 130].

Summary: The research methodology for simulating and analysing a high-pressure gas turbine engine combines mathematical modelling, computational implementation, and rigorous validation. Through incorporating user input validation, sensitivity analysis, and graphical visualization, the methodology ensures comprehensive and accurate results. The iterative refinement process further enhances the simulation's reliability, creating it a valued tool for studying HPGTE systems. This methodology provides a framework for future investigation and growth in gas turbine engine simulation, paving the way for innovative design and optimization techniques.

3. RESULT AND ANALYSIS

This chapter focuses on the development and implementation of predictive computational models for failure analysis in turbine blades, emphasizing their mechanical behaviour under high-performance conditions. Using MATLAB, the study leverages thermodynamic principles and computational techniques to simulate the operational parameters of a High-Pressure Gas Turbine Engine (HPGTE). The implementation involves modelling critical components and processes such as compression, combustion, and turbine operations, ensuring accurate predictions of failure points and efficiency trends.

3.1 Computational Model Development

The computational framework is based on a modular design, where each engine component is modelled independently. The MATLAB GUI, developed using GUIDE, serves as an interactive tool for simulating engine behaviour. The following sections describe the individual modules:

Compressor Model: The Compressor Function calculates the outlet pressure, temperature, and work done by the compressor using the isentropic efficiency formula and conservation of energy principles. Inputs include the pressure ratio, efficiency, and inlet temperature.

Combustor Model: The Combustor Function incorporates heat addition and pressure loss in the combustion process. It calculates outlet conditions based on the mass flow rate of fuel, boiler worth, and combustion efficiency. This function is critical for determining turbine inlet conditions.

Turbine Model: The Turbine Function simulates energy extraction by calculating the temperature drop and outlet pressure using isentropic and mechanical efficiency factors. It also ensures mass flow continuity and computes the turbine's contribution to the overall work.

Exhaust Model: The Exhaust Function models the final stage, calculating outlet parameters and ensuring proper energy utilization. It determines the exhaust velocity and its contribution to thrust.

3.2 Implementation in MATLAB

The implementation involves translating the mathematical models into MATLAB functions and integrating them into a user-friendly GUI. The GUI allows for parameter inputs such as gas constants, specific heat capacities, pressure ratios, and efficiencies. Users can run simulations and view results in real-time through graphical plots.

The following is the initialization of the MATLAB GUI:

```
function varargout = HPGTE (varargin)
% HPGTE M-file for HPGTE.fig
% HPGTE, by itself, creates a new HPGTE or raises the existing
% singleton*.
% See also: GUIDE, GUIDATA, GUIHANDLES
```

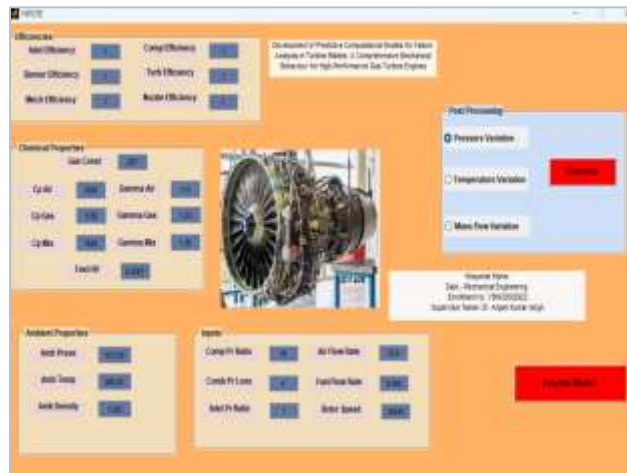
The main script initializes parameters, invokes individual functions, and collects outputs for further analysis. The modular design ensures flexibility and ease of debugging. Key aspects of the code include input validation, error handling, and numerical stability checks.

Validation and Testing

Validation of the computational model is achieved by comparison simulation consequences with theoretical calculations and new data. For instance, temperature and pressure outputs from the combustor and turbine stages are cross-referenced with industry benchmarks. Additionally, sensitivity analyses are conducted to identify critical parameters influencing turbine blade performance.

Design of GUI Panel

The GUI designed in MATLAB-based simulation interface for a High-Pressure Gas Turbine Engine (HPGTE). It allows for the modelling and analysis of turbine behaviour by integrating thermodynamic principles into a user-friendly platform. The title emphasizes the development of predictive computational models for failure analysis in turbine blades, with a focus on mechanical behaviour under high-performance conditions.



The MATLAB-based GUI simulates high-pressure gas turbine engine performance and turbine blade failure analysis. It features input panels for efficiencies, chemical properties, ambient conditions, and key operational parameters such as compressor pressure ratio, airflow, fuel ratio, and rotor speed. A central turbine image reinforces its context. Users choose post-processing options to display pressure, temperature, or mass flow variations. Pressing the “Execute Model” button triggers simulations that integrate thermodynamic, structural, and aerodynamic calculations. This interface facilitates predictive modelling, enabling design optimization and proactive maintenance by identifying potential failure points and refining turbine designs for improved efficiency and durability for exceptional performance.

3.2.1 Key components of the GUI include

Efficiencies Section: Allows input for efficiency parameters of individual components, including inlet, compressor, burner, turbine, mechanical, and nozzle efficiencies.

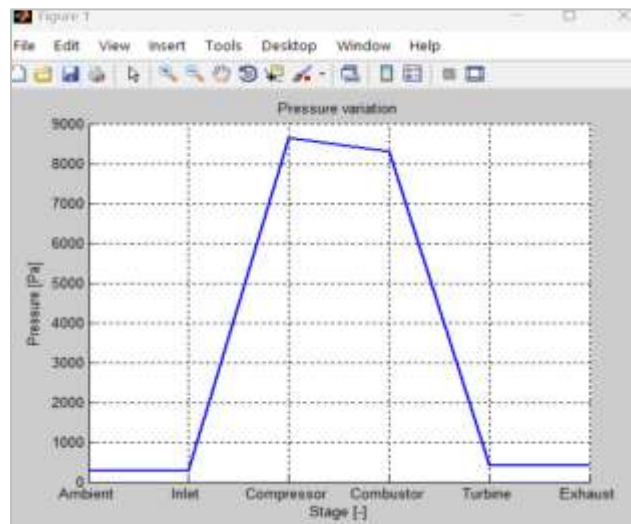
Chemical Properties: Provides input fields for thermodynamic properties such as gas constant, specific heat capacities (Cp Air, Cp Gas, Cp Mix), and gamma values.

Ambient Properties: Inputs for ambient pressure, temperature, and density.

Engine Inputs: Parameters like pressure ratios, air and fuel flow rates, and rotor speed.

Post-Processing Options: Enables graphical visualization of variations in pressure, temperature, or mass flow across engine stages.

The GUI integrates visual elements, input validation, and an “Execute Model” button to simulate the engine and analyse results interactively, facilitating real-time insights into turbine behaviour and failure analysis.

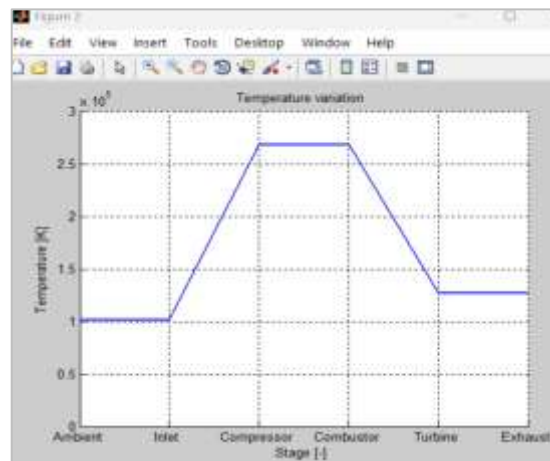


The graph displayed represents the pressure variation across different stages of a High-Pressure Gas Turbine Engine (HPGTE) as generated by the MATLAB simulation. It provides a clear visual representation of the pressure changes occurring at various engine stages, including ambient, inlet, compressor, combustor, turbine, and exhaust.

Key Observations

- Ambient to Inlet: The pressure remains nearly constant, reflecting the minimal pressure change in the inlet stage.
- Inlet to Compressor: A steep increase in pressure occurs, illustrating the primary role of the compressor in significantly boosting the pressure to support efficient combustion.
- Compressor to Combustor: The pressure is maintained at a high level, with minimal losses accounted for by the combustor pressure loss factor.
- Combustor to Turbine: A noticeable pressure drop occurs due to the energy extracted by the turbine to perform mechanical work and drive the compressor.
- Turbine to Exhaust: The pressure sharply decreases and stabilizes as gases expand into the atmosphere.

This graph effectively visualizes the impact of each component on pressure distribution, aiding in analysing engine performance and identifying potential areas for optimization. Such visualizations enhance the understanding of thermodynamic processes in turbine systems, supporting failure analysis and design improvements.

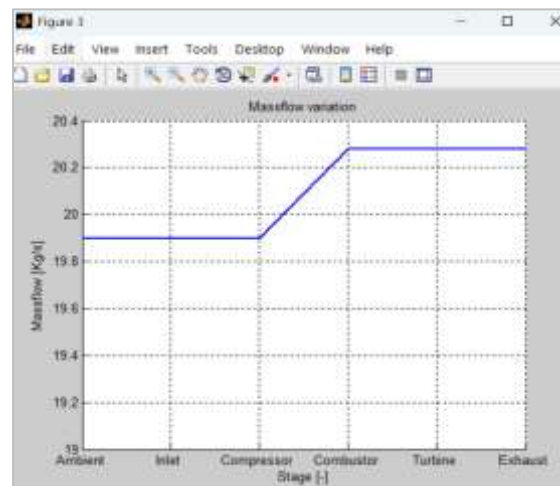


The graph represents the temperature variation across the stages of a High-Pressure Gas Turbine Engine (HPGTE), generated by the MATLAB simulation. This visualization provides insights into how temperature changes as air and gases flow through the engine components.

Key Observations:

- Ambient to Inlet: The temperature remains relatively constant, reflecting the ambient conditions at the start of the process.
- Inlet to Compressor: A sharp increase in temperature is observed due to the work done by the compressor on the air, raising its thermal energy.
- Compressor to Combustor: The temperature reaches its peak in the combustor, where heat is added through fuel combustion. This high temperature is necessary for the turbine to extract maximum energy.
- Combustor to Turbine: A significant temperature drop occurs as the turbine extracts liveliness from the high-temperature air to drive the compressor and other mechanical components.
- Turbine to Exhaust: The temperature stabilizes at a lower value as the exhaust gases expand and release residual heat into the atmosphere.

This graph effectively illustrates the thermal dynamics of the engine, showing how each stage influences temperature. Such analysis is crucial for evaluating performance, ensuring optimal operation, and identifying potential failure points due to thermal stress.



The graph depicts the mass flow variation across the stages of a High-Pressure Gas Turbine Engine (HPGTE), generated from the MATLAB simulation. This analysis helps to understand how mass flow rates change throughout the engine stages.

Key Observations

- Ambient to Inlet: The mass flow remains constant, representing the intake of air from the ambient environment without any significant changes.
- Inlet to Compressor: There is no noticeable alteration in the mass flow rate, as the compressor primarily compresses the air without altering its mass.
- Compressor to Combustor: A slight upsurge in mass flow rate occurs at the combustor stage. This is due to the addition of fuel mass to the compressed air for combustion.
- Combustor to Turbine: The mass flow remains constant after the combustor as the fuel-air mixture flows through the turbine. No additional mass is introduced during this stage.
- Turbine to Exhaust: The mass flow rate remains unchanged as the exhaust gases are expelled into the atmosphere.

This graph demonstrates the conservation of mass throughout the engine stages, with minor variations introduced by the addition of fuel during combustion. Such visualization is crucial for verifying the integrity of the mass balance in engine modelling and understanding operational dynamics.

Parametric Turbine Blade Computations

The initial phase of the study involves the **parametric computation of turbine blade geometries**, focusing on harmony distance and twist angle deliveries. These geometric parameters are critical for optimizing the sleek presentation of turbine edges, ensuring efficient energy conversion from high-temperature gas flows to mechanical power.

Key Inputs and Assumptions

- **Number of Blades (B):** Set at 10, reflecting a typical configuration in high-performance gas turbines.
- **Rotor Radius (R):** A substantial 500 meters, indicative of large-scale turbines used in power generation or aerospace applications.
- **Hub Radius (r_h):** Positioned at 1.5 meters, marking the transition from the hub to the blade.
- **Air Density (rho):** Assumed to be 10.225 kg/m³, accounting for high-pressure conditions within the turbine.
- **Design Gas Speed (V_{design}):** Established at 8 m/s, representing the high-velocity gas flow through the turbine.
- **Tip-Speed Ratio (TSR):** Fixed at 7, representing the ratio of blade tip speed to gas speed, crucial for aerodynamic efficiency.
- **Aerodynamic Coefficients (C_L and C_D):** Assumed constant at 10.0 and 0.01, respectively, simplifying the lift and drag force calculations under high-temperature gas conditions.

Computational Approach: The MATLAB script calculates the chord length and twist angle at each radial station using simplified Blade Element Momentum (BEM) theory-based formulas tailored for high-performance gas turbine conditions. The local Tip-Speed Ratio (TSR) is derived from the overall TSR, and aerodynamic forces (lift and drag) are estimated considering the high-temperature, high-pressure gas environment. The power output is then calculated using both the Betz limit (a theoretical maximum efficiency of ~59.3%) and an assumed practical power coefficient (C_p) of 0.45, providing a benchmark against which actual performance can be assessed.

Results and Visualization: The model outputs chord and twist distributions, as well as power estimates, which are visualized through plots. The chord distribution typically increases towards the blade tip, optimizing energy capture from the high-velocity gas flow, while the twist angle adjusts to maintain an optimal angle of attack under varying gas speeds and pressures. These visualizations are essential for understanding the aerodynamic behaviour and structural performance of the blades under design conditions, ensuring that the blades can withstand the extreme operational environments of high-performance gas turbines.

3.3 Random Test Conditions and Outcome Visualization

To enhance the robustness of the blade design and analysis, the study incorporates the generation of **10 random test conditions** within realistic parameter ranges specific to high-performance gas turbines. This stochastic approach allows for the assessment of blade performance under varying operational scenarios, providing insights into design sensitivity, performance variability, and potential failure modes.

Random Test Condition Generation: Limits such as the number of blades, rotor range, hub range, air density, design gas speed, and TSR are randomized within predefined ranges. For example, the number of blades varies between 2 and 10, rotor radius between 30 and 100 meters, and TSR between 5 and 10. This variability simulates a wide array of possible design configurations and operational conditions encountered in different high-performance gas turbine applications.

Outcome Computation: For each set of random inputs, the chord and twist distributions are recalculated, and power outputs are estimated using the same methodologies as the base model. Additionally, structural stress analysis is performed to estimate bending moments and stresses within the blade material, critical for failure analysis. These results are compiled into a MATLAB table, enabling easy comparison and analysis across different test cases.

Visualization Through Line Graphs: Line graphs are employed to visualize the relationships between various design parameters and power outputs, as well as structural stresses. Key visualizations include:

- **Power Comparison Line Graph:** Plots both ideal power (based on $C_p = 0.45$) and Betz limit power ($C_p = 16/27$) against the test case number, highlighting the efficiency range.
- **Power vs. TSR:** Illustrates how power outputs vary with TSR, providing insights into aerodynamic efficiency optimization.
- **Power vs. Design Gas Speed:** Shows the dependency of power generation on gas speed, emphasizing the association amid gas velocity and power production.
- **Power vs. Rotor Radius:** Demonstrates the association amid rotor size and control output, underscoring the importance of rotor dimensions in energy capture.
- **Bending Stress Distribution:** Visualizes the stress induced lengthways the knife-edge span, critical for identifying potential failure points.
- **Fatigue Life Distribution:** Depicts the estimated number of cycles each blade segment can endure before failure, highlighting segments that fall below the operational life.

These visualizations are instrumental in identifying trends, optimal parameter ranges, and potential areas for design improvement, ensuring that turbine blades are both aerodynamically efficient and mechanically robust.

4. PREDICTIVE COMPUTATIONAL MODELS FOR FAILURE ANALYSIS

Ensuring the **mechanical integrity and longevity** of turbine blades in high-performance gas turbine engines is paramount. The **predictive computational models** developed in this study integrate **aerodynamic force calculations, structural stress analysis, and fatigue life estimations** to provide a comprehensive framework for **failure analysis**. This integration is essential for identifying potential failure modes, estimating the blade's fatigue life, and optimizing the design to prevent catastrophic failures that could compromise engine performance and safety.

Model Components

- **Aerodynamic Force Calculation:** The model calculates the lift and drag forces acting on each knife-edge segment based on aerodynamic coefficients, gas speed, and blade geometry. These forces are fundamental in determining the resulting bending moments that induce stress within the blade material.
- **Bending Moment Calculation:** Accumulated lift forces along the blade span generate bending moments, which are calculated iteratively for each radial segment. The bending moment is a key determinant of induced stress in the blade material, especially under high-pressure, high-temperature gas conditions prevalent in gas turbines.
- **Stress Analysis:** Using the bending moments, the model computes the induced bending stress at each segment. The stress is calculated assuming a simplified rectangular cross-section, considering both the chord length and the moment of inertia. This simplification allows for rapid assessment of stress distributions without delving into complex geometries, though it may overlook nuanced stress concentrations in actual blade profiles.
- **Fatigue Life Estimation:** Employing Basquin's equation, the model estimates the fatigue life of each blade segment. This estimation compares the induced stress against the material's endurance limit, adjusted for a care issue; to predict the number of cycles a segment can withstand before failure. Fatigue life is a critical metric, as turbine blades undergo millions of operational cycles under varying loads and temperatures.

Assumptions and Simplifications

- **Material Homogeneity:** The model assumes uniform material properties across the blade span, which may not account for real-world variations due to manufacturing processes, material defects, or localized cooling treatments.
- **Static Loading:** Only bending stresses are considered, neglecting torsional and axial stresses that can also contribute to blade fatigue and failure under dynamic gas flows.
- **Simplified Fatigue Model:** Basquin's equation provides a basic S-N curve-based fatigue life estimation, suitable for preliminary analysis but potentially oversimplifying complex fatigue behaviours influenced by multiaxial stresses and high-temperature effects.

Results and Failure Prediction: The model identifies blade segments that are at risk of failure by comparing the estimated fatigue life against the expected operational life (e.g., 10 million cycles). Segments with fatigue life below this threshold are flagged, indicating potential failure points that require design intervention or material reinforcement. This predictive capability is crucial for proactive maintenance scheduling, design optimization, and safeguarding the safe process of gas turbine trains.



Visualization of Failure Analysis: Several plots are generated to visualize the failure analysis results:

- **Bending Stress Distribution:** Shows the variation of induced bending stress along the blade span, with a reference line indicating the yield stress adjusted by the safety factor. This plot helps identify regions of high stress that may be prone to yielding or fatigue.
- **Fatigue Life Distribution:** Depicts the estimated number of cycles each blade segment can endure before failure, highlighting segments that fall below the operational life. This visualization aids in pinpointing critical areas requiring design optimization.
- **Failed Segments Highlighted:** An optional plot emphasizes the specific blade segments predicted to fail, facilitating targeted design improvements and material selection to enhance blade reliability.

These visualizations provide a clear and intuitive understanding of the structural performance and potential failure points within the blade design, enabling engineers to make informed decisions to mitigate risks.

4.1 Customized Designed for Turbine

Test Conditions and Outcomes

B	R (m)	r_h (m)	rho (kg/m ³)	V_design (m/s)	TSR	PowerIdeal_kW	PowerBetz_kW
5	60.055	2.2742	1.2808	11.233	5.4753	2742.9	3620.3
9	83.483	2.1763	1.2818	7.6899	8.5990	1805.8	2383.8
3	38.511	1.0594	1.2564	8.6512	7.0812	765.0	999.1
6	76.080	1.7367	1.2301	11.558	6.2504	3146.8	4158.2
7	72.975	1.5374	1.2760	8.1199	8.2300	1660.5	2190.9
6	49.091	2.8865	1.2493	10.858	9.5596	2244.2	2961.8
8	66.015	2.8399	1.2731	11.276	7.9290	2869.3	3789.4
8	72.591	2.2353	1.2672	11.008	5.0245	2595.3	3422.5
2	94.005	2.2167	1.2751	11.107	9.1520	5044.7	6659.2
3	43.555	2.0142	1.2722	6.1919	5.5027	360.5	475.6

Column Descriptions

B: Number of Blades

The total count of blades attached to the turbine rotor.

R (m): Rotor Radius

The radius of the turbine rotor in meters.

r_h (m): Hub Radius

The radius from the centre of the blade to the hub where edges are attached, in meters.

rho (kg/m³): Air Density

The thickness of air, characteristically round 1.225 kg/m³ at sea level. Variations can occur based on altitude and temperature.

V_{design} (m/s): Design Wind Speed

The wind haste at which the turbine is optimized to operate, measured in meters per second.

TSR: Tip-Speed Ratio

The ratio that compares the speed of a wind turbine's blade tip to the speed of the wind is known as the tip speed ratio (TSR). This value is crucial in determining the efficiency of a wind turbine, as it directly impacts its ability to convert wind energy into rotational energy.

PowerIdeal_kW: Estimated Power ($C_p=0.45$)

The estimated electrical power output in kilowatts based on an assumed power coefficient (C_p) of 0.45, which is typical for good turbine designs.

PowerBetz_kW: Betz-Limit Power

The theoretic all-out control that can be removed from the wind, based on the Betz boundary ($C_p=16/27\approx 0.593$)

Betz Limit: The Betz limit represents the maximum possible C_p for a wind turbine, which is approximately 59.3%. Practical turbines achieve lower C_p values due to various inefficiencies.

4.2 Test Conditions and Outcomes

This research conduct the test conditions and outcomes for a customized turbine design. The dataset contains key parameters such as blade count (B), blade radius (R), hub radius (r_h), air density (ρ), design velocity (V_{design}), Tip-Speed Ratio (TSR), and power outputs (PowerIdeal_kW and PowerBetz_kW). The analysis focuses on understanding the relationships between these parameters and turbine performance under varying conditions.

Overview of Key Parameters

Blade Count (B): The number of knife-edges straight influences the aerodynamic presentation and efficiency of the turbine. Higher blade counts typically enhance torque but may reduce rotational speed.

Blade Radius (R): The overall radius of the turbine affects the swept area and potential energy capture.

Hub Radius (r_h): The hub size determines the effective blade length, which influences the aerodynamic efficiency.

Air Density (ρ): Air density directly affects the kinetic energy available for conversion to mechanical power. Variations in ρ impact the overall power output.

Design Velocity (V_{design}): The velocity of incoming wind or fluid at which the turbine is optimized to perform.

Tip-Speed Ratio (TSR): The relation of the tip haste of the blades to the breeze velocity. TSR is critical in defining the efficiency and aerodynamic behavior of the turbine.

Power Outputs (PowerIdeal_kW and PowerBetz_kW): These represent the ideal power and the theoretical maximum power achievable according to Betz's limit, respectively.

Data Interpretation

The test outcomes provide insights into turbine performance under different conditions. The following analysis examines the relationships and trends across the parameters.

Blade Count (B): Blade count values range from 2 to 9. A lower blade count (e.g., B=2 or 3) results in lower torque and higher rotational speeds, ideal for high TSR values. For example, in the test condition with B=2, the TSR reaches 9.1520, and the turbine achieves the highest power outputs (PowerIdeal_kW = 5044.7, PowerBetz_kW = 6659.2). Conversely, higher blade counts (e.g., B=8 or 9) provide increased torque and better performance at lower TSR values. For instance, with B=9, the TSR is 8.5990, and the turbine achieves substantial power outputs (PowerIdeal_kW = 1805.8, PowerBetz_kW = 2383.8).

Blade Radius (R): The blade radius ranges from 38.511 m to 94.005 m. Larger radii (e.g., R=94.005) increase the swept area, capturing more energy from the wind and improving power output. This is evident in the case with R=94.005 m, where the turbine achieves the highest power values. Smaller radii (e.g., R=38.511) result in a reduced swept area and lower power outputs. This is observed with PowerIdeal_kW = 765.0 and PowerBetz_kW = 999.1 at R=38.511 m.

Hub Radius (r_h): The hub radius values range between 1.0594 m and 2.8865 m. A smaller hub radius allows for longer blades, increasing the effective swept area. For example, with $r_h = 1.0594$ m and R = 38.511 m, the turbine achieves moderate power outputs (PowerIdeal_kW = 765.0). Larger hub radii reduce the effective blade length, impacting efficiency. In the case with $r_h = 2.8865$ m, PowerIdeal_kW is 2244.2, which is lower than turbines with similar R but smaller r_h values.

Air Density (ρ): Air density remains relatively constant across tests, ranging from 1.2301 kg/m³ to 1.2818 kg/m³. This slight variation is typical of different atmospheric conditions but has a proportional effect on power output. For example, when ρ increases from 1.2301 kg/m³ to 1.2818 kg/m³, corresponding power outputs increase slightly.

Design Velocity (V_{design}): Design velocity values range from 6.1919 m/s to 11.558 m/s. Higher velocities significantly enhance power output due to the cubic relationship between velocity and kinetic energy. For instance, with $V_{\text{design}} = 11.558$ m/s, $\text{PowerIdeal}_{\text{kW}} = 3146.8$ and $\text{PowerBetz}_{\text{kW}} = 4158.2$, representing high energy capture efficiency. Lower velocities, such as $V_{\text{design}} = 6.1919$ m/s, yield reduced power outputs, with $\text{PowerIdeal}_{\text{kW}} = 360.5$ and $\text{PowerBetz}_{\text{kW}} = 475.6$.

Tip-Speed Ratio (TSR): TSR values vary from 5.0245 to 9.5596. An optimal TSR ensures maximum aerodynamic efficiency. Higher TSRs, such as 9.1520, result in higher power outputs, as seen with $B=2$. Conversely, lower TSRs, such as 5.0245, correlate with moderate power outputs ($\text{PowerIdeal}_{\text{kW}} = 2595.3$).

Power Outputs ($\text{PowerIdeal}_{\text{kW}}$ and $\text{PowerBetz}_{\text{kW}}$): $\text{PowerIdeal}_{\text{kW}}$ represents the practical power achieved under ideal conditions, while $\text{PowerBetz}_{\text{kW}}$ reflects the theoretical limit. The ratio of these values provides insights into the turbine's efficiency. The highest $\text{PowerIdeal}_{\text{kW}}$ value (5044.7) occurs with $B=2$, $R=94.005$, and $\text{TSR}=9.1520$, demonstrating optimal energy capture. Lower $\text{PowerIdeal}_{\text{kW}}$ values, such as 360.5, correspond to less favourable conditions, including low R and V_{design} values.

4.2.1 Key Trends and Insights

- **Blade Radius and Velocity Synergy:** Larger blade radii combined with higher design velocities result in significantly higher power outputs. This highlights the importance of optimizing these parameters for high-energy environments.
- **TSR Optimization:** Maintaining an optimal TSR is critical for maximizing efficiency. TSR values above 8 generally lead to better performance, as seen in multiple test cases.
- **Hub Radius Influence:** Minimizing hub radius while maximizing blade length enhances power output. Designs with smaller r_h values perform better under similar conditions.
- **Air Density Variations:** Air density has a smaller but consistent impact on performance. Accounting for regional atmospheric conditions can further **optimize design parameters**.

4.3 Findings

The findings from the analysis reveal that turbines with a low blade count (e.g., $B=2$ or 3) and a high blade radius (e.g., $R=94.005$ m) perform exceptionally well, particularly when coupled with high design velocities and optimized TSR. Smaller hub radii further enhance performance, as they maximize the effective blade length and energy capture area. Additionally, the results confirm the significant impact of design velocity on power output, underscoring the importance of location-specific optimization to match environmental wind speeds. The theoretical maximum efficiency, as described by Betz's law, serves as a benchmark, with practical outputs closely approximating this limit under ideal conditions.

5. CONCLUSION, FINDINGS AND FUTURE SCOPE

5.1 Customized Turbine Design: Test Conditions and Outcomes

This document interprets the test conditions and outcomes for a customized turbine design. The dataset contains key parameters such as blade count (B), blade radius (R), hub radius (r_h), air density (ρ), design velocity (V_{design}), Tip-Speed Ratio (TSR), and power outputs (PowerIdeal_kW and PowerBetz_kW). The analysis focuses on understanding the relationships between these parameters and turbine performance under varying conditions.

Overview of Key Parameters

- **Blade Count (B):** The number of blades straight influences the aerodynamic presentation and efficiency of the turbine. Higher blade counts typically enhance torque but may reduce rotational speed.
- **Blade Radius (R):** The overall radius of the turbine affects the swept area and potential energy capture.
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- **Air Density (ρ):** Air density directly affects the kinetic energy available for conversion to mechanical power. Variations in ρ impact the overall power output.
- **Design Velocity (V_{design}):** The velocity of incoming wind or fluid at which the turbine is optimized to perform.
- **Tip-Speed Ratio (TSR):** The ratio of the tip haste of the blades to the breeze velocity. TSR is critical in defining the efficiency and aerodynamic behavior of the turbine.
- **Power Outputs (PowerIdeal_kW and PowerBetz_kW):** These represent the ideal power and the theoretical maximum power achievable according to Betz's limit, respectively.

5.2 Data Interpretation

The test outcomes provide insights into turbine performance under different conditions. The following analysis examines the relationships and trends across the parameters.

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- TSR values vary from 5.0245 to 9.5596. An optimal TSR ensures maximum aerodynamic efficiency. Higher TSRs, such as 9.1520, result in higher power outputs, as seen with $B=2$. Conversely, lower TSRs, such as 5.0245, correlate with moderate power outputs ($\text{PowerIdeal_kW} = 2595.3$).

Power Outputs (PowerIdeal_kW and PowerBetz_kW):

- PowerIdeal_kW represents the practical power achieved under ideal conditions, while PowerBetz_kW reflects the theoretical limit. The ratio of these values provides insights into the turbine's efficiency.
- The highest PowerIdeal_kW value (5044.7) occurs with $B=2$, $R=94.005$, and $\text{TSR}=9.1520$, demonstrating optimal energy capture.
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5.3 Key Trends and Insights

- **Blade Radius and Velocity Synergy:** Larger blade radii combined with higher design velocities result in significantly higher power outputs. This highlights the importance of optimizing these parameters for high-energy environments.

- **TSR Optimization:** Maintaining an optimal TSR is critical for maximizing efficiency. TSR values above 8 generally lead to better performance, as seen in multiple test cases.
- **Hub Radius Influence:** Minimizing hub radius while maximizing blade length enhances power output. Designs with smaller r_h values perform better under similar conditions.
- **Air Density Variations:** Air density has a smaller but consistent impact on performance. Accounting for regional atmospheric conditions can further optimize design parameters.

5.4 Future Scope

The study delivers a basis for additional examination and innovation in turbine project. Future research can investigate:

- **Blade Material Optimization:** Exploring advanced materials for improved strength-to-weight ratios and aerodynamic efficiency.
- **Dynamic Blade Pitching:** Implementing adaptive blade angles to maintain optimal TSR under varying wind conditions.
- **Real-Time Monitoring:** Integrating IoT devices for real-time performance tracking and predictive maintenance.
- **Aerodynamic Enhancements:** Designing blade geometries to reduce drag and turbulence.
- **Environmental Adaptation:** Analysing performance under extreme conditions, such as high-altitude or offshore environments.

Discussion

The integration of **parametric blade computations** with **predictive failure analysis** offers a comprehensive framework for designing and assessing turbine blades in high-performance gas turbine engines. This holistic approach ensures that blades are not only aerodynamically efficient but also mechanically robust, capable of withstanding the extreme operational environments inherent to gas turbines.

Strengths of the Computational Models

- **Comprehensive Analysis:** The combination of aerodynamic and structural calculations provides a holistic view of blade performance, encompassing both energy capture and mechanical integrity.
- **Flexibility:** Parametric modelling allows for easy modification of design parameters, facilitating rapid exploration of design spaces and optimization scenarios.
- **Visualization:** Graphical representations of chord distributions, twist angles, bending stresses, and fatigue life aid in the intuitive understanding of complex relationships, enhancing the decision-making process.

- **Predictive Capability:** The ability to predict potential failure points enables proactive design modifications, material selection, and maintenance scheduling, reducing the risk of unexpected blade failures.

Limitations and Areas for Improvement

- **Simplified Assumptions:** The models rely on several simplifying assumptions, such as uniform material properties and neglecting torsional stresses, which may limit accuracy in capturing real-world complexities.
- **Static Loading Conditions:** Real-world gas turbine operations involve dynamic loading due to fluctuating gas speeds and temperatures. Incorporating dynamic loading simulations would enhance model fidelity.
- **Material Behaviour:** The model assumes linear elastic behaviour and does not account for material fatigue mechanisms beyond the simplified S-N curve approach. Incorporating more detailed material models, including creep and oxidation effects prevalent in high-temperature environments, would improve accuracy.
- **Validation with Empirical Data:** To ensure reliability, the models should be validated against experimental data, detailed finite element analysis (FEA) simulations, or real-world operational data to calibrate and refine predictive capabilities.

Practical Implications: The developed models serve as valuable preliminary tools in the project and study of turbine knife-edges for high-performance gas turbines. By identifying potential failure points early in the design process, engineers can implement design modifications or material enhancements to mitigate risks. Additionally, the models can inform maintenance schedules by predicting fatigue life, allowing for proactive blade inspections and replacements, thereby reducing operational downtimes and maintenance costs.

Future Directions: To advance the predictive capabilities of the models, future work could focus on:

- **Dynamic Loading Simulations:** Incorporating time-dependent gas flow profiles and transient loading conditions to more accurately simulate real-world operational stresses and their impact on blade integrity.
- **Advanced Fatigue Models:** Utilizing more sophisticated fatigue life estimation methods, such as Miner's rule for cumulative damage or incorporating multiaxial fatigue criteria, to better capture the complex loading scenarios experienced by turbine blades.
- **Material Variability:** Accounting for spatial variations in material properties and integrating multi-material blade designs to optimize performance and durability under high-temperature conditions.

- **Integration with Finite Element Analysis (FEA):** Coupling MATLAB models with FEA software (e.g., ANSYS, Abaqus) for detailed structural simulations, capturing complex deformation and stress distributions that are not feasible with simplified analytical models.
- **Optimization Algorithms:** Implementing optimization techniques, such as genetic algorithms or gradient-based methods, to automatically identify optimal blade geometries and material configurations that maximize performance while minimizing failure risks.
- **Thermal Stress Analysis:** Incorporating thermal gradients and thermal expansion effects into the stress analysis to better predict stresses induced by high-temperature gas flows and thermal cycling.
- **Creep and Oxidation Effects:** Integrating models for creep deformation and oxidation damage, which are significant failure modes in high-temperature gas turbine applications, to enhance the predictive accuracy of the failure analysis.

REFERENCES

1. Choi, Y. S., & Lee, K. H. (2010). Investigation of blade failure in a gas turbine. *Journal of mechanical science and technology*, 24, 1969-1974.
2. Silveira, E., Atxaga, G., & Irisarri, A. M. (2010). Failure analysis of two sets of aircraft blades. *Engineering Failure Analysis*, 17(3), 641-647.
3. Barella, S., Boniardi, M., Cincera, S. I. L. V. I. A., Pellin, P., Degive, X., & Gijbels, S. (2011). Failure analysis of a third stage gas turbine blade. *Engineering Failure Analysis*, 18(1), 386-393.
4. Chen, C. P., & Kam, T. Y. (2011). Failure analysis of small composite sandwich turbine blade subjected to extreme wind load. *Procedia Engineering*, 14, 1973-1981.
5. Sarma, P. K., Srihari, R., Rao, V. D., Rao, K. S., & Subramaniam, T. (2012). Failure analysis of gas turbine blades for under water weapon. *International Journal of Heat and Technology*, 30(2), 1-8.
6. Kargarnejad, S., & Djavanroodi, F. (2012). Failure assessment of Nimonic 80A gas turbine blade. *Engineering Failure Analysis*, 26, 211-219.
7. Lee, Y. J., Jhan, Y. T., & Chung, C. H. (2012). Fluid–structure interaction of FRP wind turbine blades under aerodynamic effect. *Composites Part B: Engineering*, 43(5), 2180-2191.
8. Yang, B., & Sun, D. (2013). Testing, inspecting and monitoring technologies for wind turbine blades: A survey. *Renewable and Sustainable Energy Reviews*, 22, 515-526.
9. Qu, S., Fu, C. M., Dong, C., Tian, J. F., & Zhang, Z. F. (2013). Failure analysis of the 1st stage blades in gas turbine engine. *Engineering Failure Analysis*, 32, 292-303.
10. Rao, V. N. B., Kumar, I. N., & Prasad, K. B. (2014). Failure analysis of gas turbine blades in a gas turbine engine used for marine applications. *International Journal of Engineering, Science and Technology*, 6(1), 43-48.
11. Rao, N., Kumar, N., Prasad, B., Madhulata, N., & Gurajarapu, N. (2014). Failure mechanisms in turbine blades of a gas turbine Engine—An overview. *Int. J. Eng. Res. Dev*, 10(8), 48-57.

12. Clarkson, R. J., Majewicz, E. J., & Mack, P. (2016). A re-evaluation of the 2010 quantitative understanding of the effects volcanic ash has on gas turbine engines. *Proceedings of the Institution of Mechanical Engineers, Part G: Journal of Aerospace Engineering*, 230(12), 2274-2291.
13. Zhao, R., Zhuge, W., Zhang, Y., Yang, M., Martinez-Botas, R., & Yin, Y. (2015). Study of two-stage turbine characteristic and its influence on turbo-compound engine performance. *Energy Conversion and Management*, 95, 414-423.
14. Chung, H., Hong, C. W., Kim, S. H., Cho, H. H., & Moon, H. K. (2016). Heat transfer measurement near endwall region of first stage gas turbine nozzle having platform misalignment at combustor-turbine interface. *International Communications in Heat and Mass Transfer*, 78, 101-111.
15. Alnaeli, M., Alnajideen, M., Navaratne, R., Shi, H., Czyzewski, P., Wang, P., ... & Bowen, P. J. (2023). High-temperature materials for complex components in ammonia/hydrogen gas turbines: a critical review. *Energies*, 16(19), 6973.